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Study of deflections of bending layered structures taking into account transverse shear deformations

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Study of deflections of bending layered structures taking into account transverse shear deformations

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Abstract: The article considers the influence of shear stresses on the deformation of structural elements subject to bending. It is known that the structural element subject to bending is a beam, and the main problem is to check its rigidity. To do this, it is necessary to determine the displacements that occur under the action of external forces. This problem is solved based on the integration of the main differential equation of the curved axis of the beam. However, in general, the bending of the beam is also significantly affected by shear stresses that occur on the surfaces of its cross section. The shear deformation caused by these stresses, in some cases, can have a significant effect on the deformation of the beam, that is, on its rigidity. The paper considers the study of a three-layer rod consisting of a lightweight porous material, such as foam plastic, called a filler, connected on the outer surfaces with thin metal sheets (bearing layers).

Key words: deformation, beam, shear, layers, bearing layer, rigidity, filler, deflection, shear stresses, bending moments, rod, element, displacement function, stress function, diagrams, coefficient.

INTRODUCTION

Let us consider, in contrast to cases, when determining deflections, in addition to the deformation of curvature created by bending moments, we take into account the shear of the beam elements.

The shear deformation of the rod element is created by transverse forces $-Q$, which are caused by the average shear of the element [4,5,6].

$$\gamma_{av} = \frac{kQ}{GA} \quad (1)$$

where k is a coefficient that takes into account the uneven distribution of tangential stresses in the cross-section; its value depends on the cross-section of the beam.

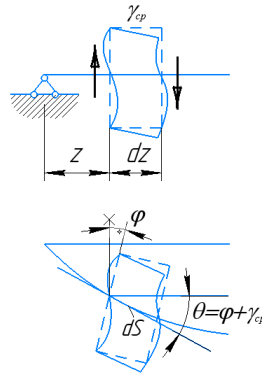


FIGURE 1. General view of a rotated cross-section of a beam after deformation, considering shear deformation.

LITERATURE REVIEW AND METHODS

If we still denote the angle of rotation of the cross section by φ , and the angle of inclination of the tangent to the axis of the bent beam by θ , then it is easy to see that the segment of the axis dS as an element of the tangent curve $v = v(z)$ in addition to the angle φ will rotate due to the shift by the angle γ_{av} so that the total angle of inclination of the tangent θ will be.

$$\theta = \varphi + \gamma_{av} \quad (2)$$

Since the cross-section will not be normal to the axis of the beam when taking into account the shifts [5,6,7].

Based on the equality $\theta = \varphi'$, instead of $\varphi = \frac{dv}{dz} = v'(a)$ we get.

$$\varphi + \gamma_{av} = v' \quad (3)$$

and a system of differential equations

$$\begin{aligned} \frac{d\varphi}{dz} &= -\frac{M}{EJ} \\ \frac{d\varphi}{dz} &= \varphi \end{aligned}$$

taking into account the shifts will have the form

$$\left. \begin{aligned} \frac{d\varphi}{dz} &= -\frac{M}{EJ} \\ \frac{dv}{dz} &= \varphi + \frac{kQ}{GA} \end{aligned} \right\} \quad (4)$$

Substituting φ from the second line into the first, we obtain instead the second-order equation $\frac{d^2v}{dz^2} = -\frac{M}{EJ}$ taking into account the shifts.

$$\frac{d^2v}{dz^2} = -\frac{M}{EJ} + \frac{d}{dz} \left(\frac{kQ}{GA} \right) \quad (5)$$

When integrating equations (4) or (5), it should be borne in mind that two separate displacement functions are subject to determination: the deflection function $v(z)$ and the section rotation angle function $\varphi(z)$ the latter are no longer related by deflections (a), as was the case without taking into account the shifts. Their dependence is determined by equality. (2) This creates its own peculiarities in the formulation of boundary conditions and conditions of

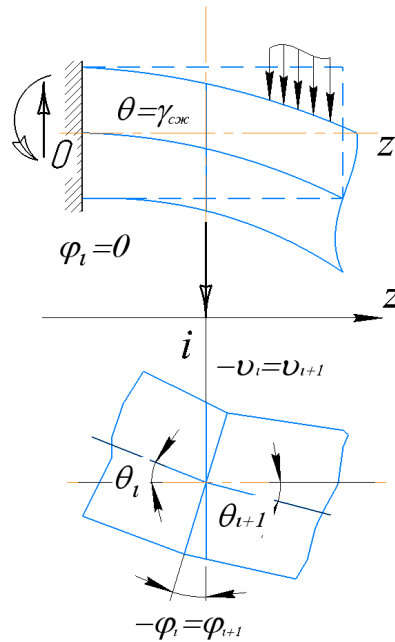


FIGURE 2. Example for determining the deflection of a homogeneous cantilever beam with a rectangular cross-section, taking shear deformation into account.

continuity of displacements at the boundaries of the integration sections. For example, in the embedment, the boundary conditions at $z=0$ will be: 1) $v(0)=0$ and 2) $\varphi(0)=0$. In this case, from the second condition and equality (2) it follows that the tangent in the embedment will turn by an angle of $\theta = \gamma_{\text{сдв}}$.

At the boundary of the sections at the i -th point the conditions of continuity of displacements will be $v_i = v_{i+1}$ and $\varphi_i = \varphi_{i+1}$. In this case the angles of inclination of the tangents can be different $\theta_i \neq \theta_{i+1}$, if $\theta_i = \theta_{i+1}$.

Example. Find the deflections of a homogeneous cantilever beam of rectangular cross-section taking into account the shear deformation from a uniformly distributed load. (Fig. 3)

Solution. We use the system of equations (4). From the first equation we find $\varphi = -\int_0^z \frac{Mdz}{EJ} + \varphi_0$ from the second equation $v = \int_0^z \varphi dz + \int_0^z \frac{kQ}{GA} dz + v_0$

In the case under consideration, $M = \frac{ql^2}{2} - \frac{qz^2}{2} + qlz$ and $Q = ql - qz$, in addition, in the seal $v_0=0$ $\varphi_0=0$, therefore, for the expressions φ and v we obtain the following expression

$$\varphi = \frac{ql^2 z}{2EJ} - \frac{qlz^2}{2EJ} + \frac{qz^2}{6EJ}; \quad v = \frac{ql^2 z^2}{4EJ} - \frac{qlz^3}{6EJ} + \frac{qz^4}{24EJ} + \frac{k}{GA} \left(qlz - \frac{qz^2}{2} \right)$$

The obtained expressions for the deflections v can be represented as the sum of two functions $v = v_M + v_Q$

where $v = \frac{ql^2 z^2}{4EJ} - \frac{qlz^3}{6EJ} + \frac{qz^4}{24EJ}$ - deflections caused by bending moments $v_Q = \frac{k}{GA} \left(qlz + \frac{qz^2}{2} \right)$ - deflections from shear deformations caused by transverse forces.

The diagram of v_Q and v_M is shown in Fig. 3. Their sum will give the general line of deflections.

Let's calculate the deflection at the end of the beam $v_Q(l) = f_Q$ and $v_M(l) = f_M$ compare them quantitatively. At $z=l$ we find f_Q, f_M and their ratios:

$$f_Q = \frac{kql^2}{2GA}; \quad f_M = \frac{ql^4}{8GA}; \quad \frac{f_Q}{f_M} = 4 \frac{E}{G} \frac{J}{Al^2} k \quad (6)$$

In the case of a homogeneous beam we have $E = 2(1+\mu)G$; $J = bh^3/12$; $A = bh$, $k = 6/5$. Sloping $l/h = 5$ and $\mu = 0,25$ we get

$$\frac{f_Q}{f_M} = \frac{12}{15}(1-\mu) \frac{h^2}{l^2} = \frac{12}{15} \cdot 1,25 \frac{1}{5^2} = \frac{1}{25}$$

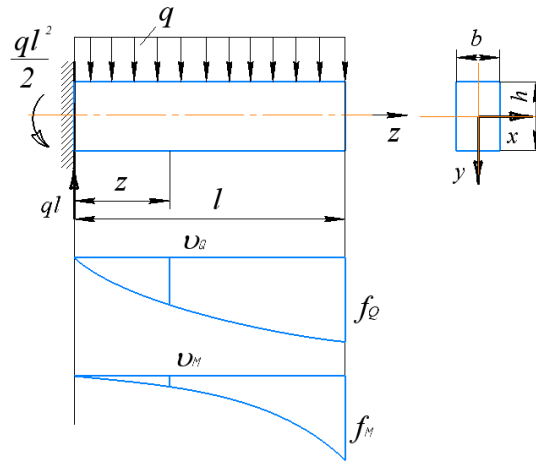


FIGURE 3. Deflection of the beam from shear deformations v_Q and from bending v_M

i.e. the deflection caused by shear deformations is 25 times less than the deflection caused by bending moments. The shear deformation can be justifiably neglected, as it was accepted according to the hypotheses of Kirchhoff, they can be neglected except for layered structures. But in engineering and construction, multilayer elements of structures are widely used [1,2,3,4].

RESULTS

Let us consider a three-layer rod consisting of a lightweight porous material, such as foam plastic, called a filler, connected on the outer surfaces with thin metal sheets (bearing layers). Three-layer panels are usually used, which have high heat-insulating and bearing properties and, in addition, very low weight. Let us estimate the effect of shear deformations in such a three-layer beam, using the calculation scheme and formulas obtained in the example in Fig. 4. The modulus of elasticity of the filler is many times less than the modulus of elasticity of the bearing layers. Therefore, it is considered that the entire bending moment in the section is taken by the bearing layers, and the filler perceives only the shear stresses τ , which in this case will be constant across its thickness. Then, in formulas (6), the rigidity EJ will relate only to the bearing layers and will be

$$EJ = E2\delta(h/2)^2 = E\delta h^2/2$$

where E – modulus of elasticity of the material of the supporting (layers) sheets
 δ – sheet thickness

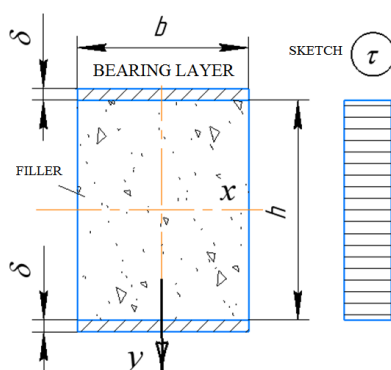


FIGURE 4. Calculation diagram of a three-layer rod and the law of shear stress distribution in the core material.

At the same time, the shear rigidity GA will relate only to the filler and will be $GA=Gbh$, where G is the filler shear modulus. Due to the uniformity of the distribution of τ across the filler thickness, the coefficient k in formula (1).

CONCLUSION

Substituting the given values of EJ and GA into formula (6) for f_Q/f_M , we obtain the desired ratio of the deflection from transverse forces to the deflection from bending moments of a three-layer beam:

$$\frac{f_Q}{f_M} = 2 \frac{E\delta h^2}{Ghl^2}$$

Let $h/l=1/5$; $\delta/h=10^{-2}$ и $E/G=10^3$, $f_Q/f_M=0,8$ i.e. shear deformations increase the deflection f_M from bending moments by 80% and in this case shear deformations should in no case be neglected.

Usually multilayer elements of structures, road and airfield pavements are calculated taking into account shear deformation. These issues are considered in detail in the works.

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